Master Equations

1 Problem Setup

Assume Quasi-1D, steady, no body forces and negligible viscous work flow, as shown below:



Figure 1: Problem Setup

2 Mass Conservation

Because we know the flow is steady:

$$\dot{m} = const = \rho uA \tag{1}$$

$$0 = d(\rho u A) \tag{2}$$

$$0 = uAd\rho + \rho Adu + \rho udA \tag{3}$$

Divide it by ρuA :

$$0 = \frac{d\rho}{\rho} + \frac{du}{u} + \frac{dA}{A} = \frac{d\rho}{\rho} + \frac{1}{2}\frac{d(u^2)}{u^2} + \frac{dA}{A}$$
(4)

Recall the continuity equation:

$$\frac{D\rho}{Dt} + \rho(\nabla \cdot \underline{\boldsymbol{u}}) = 0 \tag{5}$$

If steady flow:

$$\frac{D\rho}{Dt} = \frac{d\rho}{dt} + \left[\frac{d(\rho u)}{dx} + \frac{d(\rho v)}{dy} + \frac{d(\rho w)}{dz}\right]$$
(6)

Because we assume 1D:

$$\frac{d(\rho u)}{dx} = 0\tag{7}$$

Also due to constant mass flow rate, this in other words means:

$$\frac{dA}{dx} = 0 \tag{8}$$

Therefore we can conclude that quasi steady only valid if area changes slowly.

3 Momentum Conservation



Figure 2: Momentum Conservation

Same conditions, recall the expression for momentum conservation:

$$\sum F = (\dot{m}u)_{net} \tag{9}$$

We define **right direction as positive direction**, then:

$$\sum F = -\tau_x L_p dx + F_p \tag{10}$$

Here τ_x is the shear stress, with the unit as F/A, and the unit of $L_p dx$ is A. For the force from pressure F_p , we divide it into 4 parts:

1. Surface 1:

$$(F_p)_{s1} = pA \tag{11}$$

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2. Surface 2,4: This one is tricky. Because we only want the momentum in x direction, so we need to use the normal cross section, which is $-\frac{dA}{2}$, here dA is negative. Also, we assume the pressure acting at the middle point of the surface as $p + \frac{dp}{2}$. Therefore:

$$(F_p)_{s2+s4} = 2 \times -(p + \frac{dp}{2})(-\frac{dA}{2}) = (p + \frac{dp}{2})dA$$
(12)

3. Surface 3:

$$(F_p)_{s3} = -(p+dp)(A+dA)$$
 (13)

Now we add all the surfaces:

$$F_p = pA + (p + \frac{dp}{2})dA + -(p + dp)(A + dA)$$
(14)

Assume the second order term dpdA as 0, then we have:

$$F_p = -Adp \tag{15}$$

Therefore, we have:

$$-\tau_x L_p dx - A dp = (\dot{m}u)_{net} = \dot{m} du = \rho u A du \tag{16}$$

Rearrange and divide it by pA:

$$\frac{\rho}{p}udu + \frac{\tau_x}{p}\frac{L_p}{A}dx + \frac{dp}{p} = 0 \tag{17}$$

$$\frac{\rho}{p}\frac{u^2}{2}\frac{du^2}{u^2} + \frac{\tau_x}{p}\frac{L_p}{A}dx + \frac{dp}{p} = 0$$
(18)

4 Energy Conservation



Figure 3: Energy Conservation

Recall the first law:

$$\partial q = dh_o = dh + d(\frac{u^2}{2}) = c_p dT + \frac{1}{2} du^2$$
 (19)

Therefore:

$$\frac{\partial q}{c_p T} = \frac{dT}{T} + \frac{1}{2c_p T} du^2 \tag{20}$$

Recall that:

$$c_p = \frac{\gamma R}{\gamma - 1} \tag{21}$$

Finally we have:

$$\frac{dT}{T} = \frac{\partial q}{c_p T} - \frac{\gamma - 1}{2} \frac{u^2}{\gamma RT} \frac{du^2}{u^2}$$
(22)

5 Master Equations

Recall that:

$$M^2 = \frac{u^2}{\gamma RT}, \ \frac{p}{\rho} = RT \tag{23}$$

We can rewrite the previous equations in terms of Mach number. Mass:

$$\frac{d\rho}{\rho} + \frac{1}{2}\frac{d(u^2)}{u^2} + \frac{dA}{A} = 0$$
(24)

Momentum:

$$M^{2} \frac{\gamma}{2} \frac{du^{2}}{u^{2}} + \frac{\tau_{x}}{p} \frac{L_{p}}{A} dx + \frac{dp}{p} = 0$$
⁽²⁵⁾

Energy:

$$\frac{dT}{T} = \frac{\partial q}{c_p T} - \frac{\gamma - 1}{2} M^2 \frac{du^2}{u^2}$$
(26)

Also from ideal gas law:

$$dp = d(\rho RT) = \rho R dT + RT d\rho \tag{27}$$

Therefore:

$$\frac{dp}{p} = \frac{\rho R}{p} dT + \frac{RT}{p} d\rho \tag{28}$$

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$$\frac{dp}{p} = \frac{dT}{T} + \frac{d\rho}{\rho} \tag{29}$$

Similarly, we have:

$$d(u^2) = d(\gamma RTM^2) = \gamma M^2 R dT + M^2 RT d\gamma + \gamma RT dM^2$$
(30)

Divide it by u^2 , we have:

$$\frac{du^2}{u^2} = \frac{dT}{T} + \frac{d\gamma}{\gamma} + \frac{dM^2}{M^2}$$
(31)

Therefore, we have 5 equations and 5 unknowns (M, ρ, u, p, T) , and 3 given inputs:

- 1. Area change: dA
- 2. Shear stress/friction: τ_x
- 3. Heat transfer: ∂q

We only get general analytic solutions if we **specify one input**, and let the other **two be 0**, so we have 5 equations 5 unknowns.